

Smart Mitigation of flow-induced Acoustic Radiation and
Transmission for reduced Aircraft, Surface transport,
Workplaces and wind energy noise



Development Rod-Linear Cascade Model for Fan-Wake/OGV Interaction Noise Studies

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TU Delft/3DS Workshop, 14 September 2018

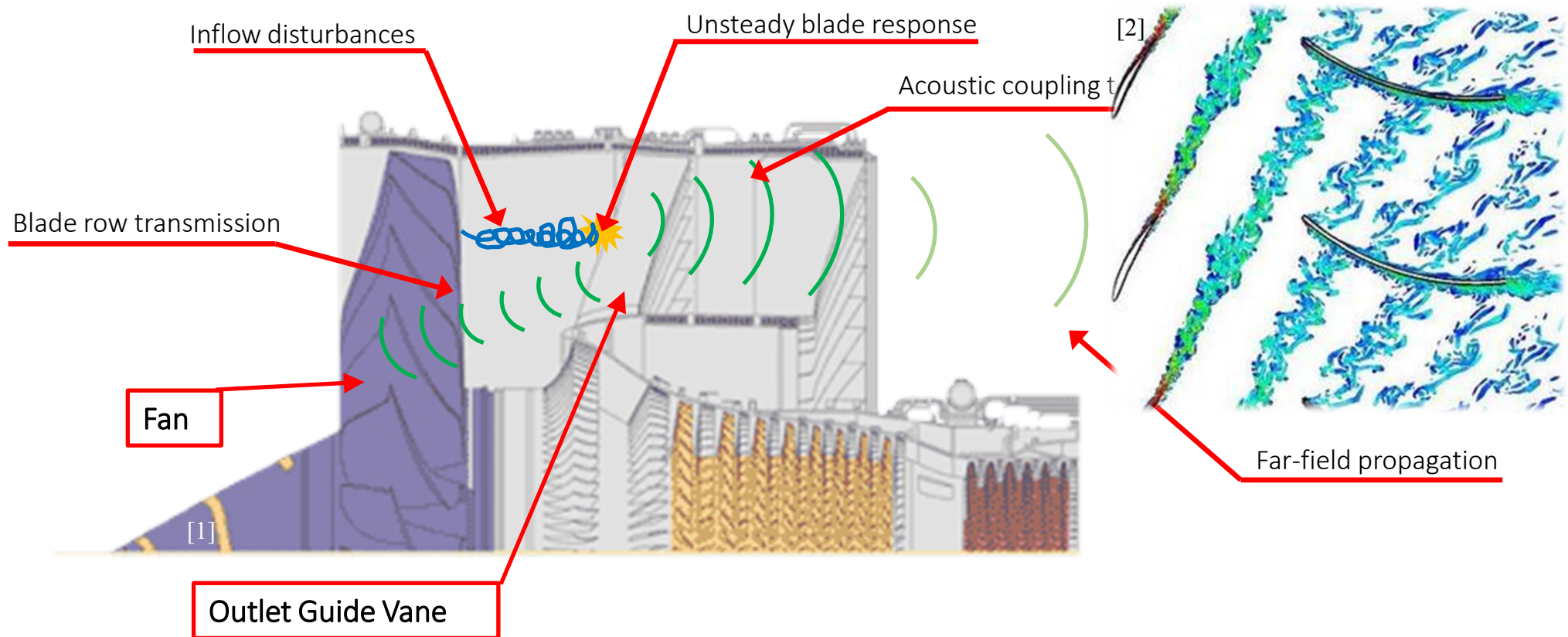


H2020 MARIE SKŁODOWSKA-CURIE ACTIONS

- Introducing The Rod – Linear Cascade Test Rig
- Preliminary Computational Results using PowerFLOW
- Noise Mitigation Strategies and Outlook
- Q&A session



I. ROD – LINEAR CASCADE



A simplified **test model** which replicates the turbulence impingement mechanism would be advantageous for **parametric studies** and **noise mitigation applications**.

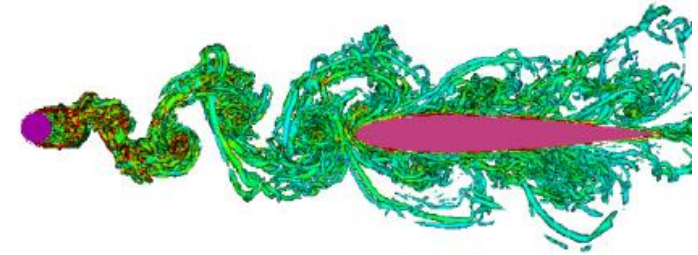
* Turbulence Impingement Noise

[1] <https://www.behance.net/gallery/27888995/How-does-a-turbofan-engine-work>

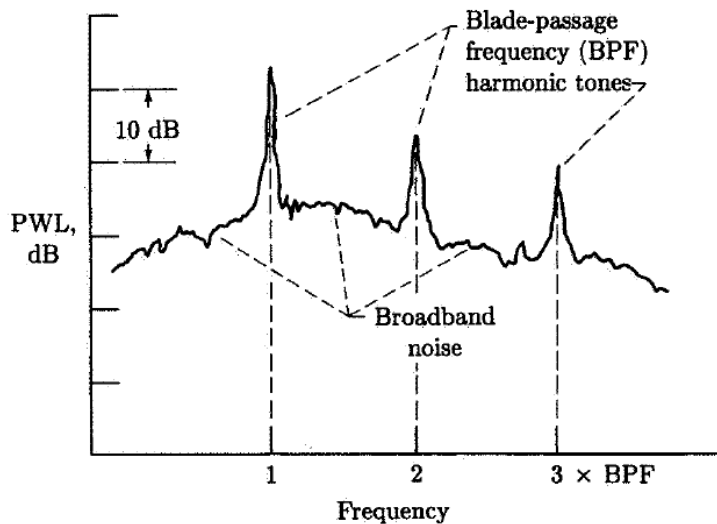
[2] Enghardt, L. Improvement of Fan Broadband Noise Prediction: Experimental Investigation and Computational Modelling. *Final Project Report: Proband-DLR-WP1-Task, 1*. 2008.



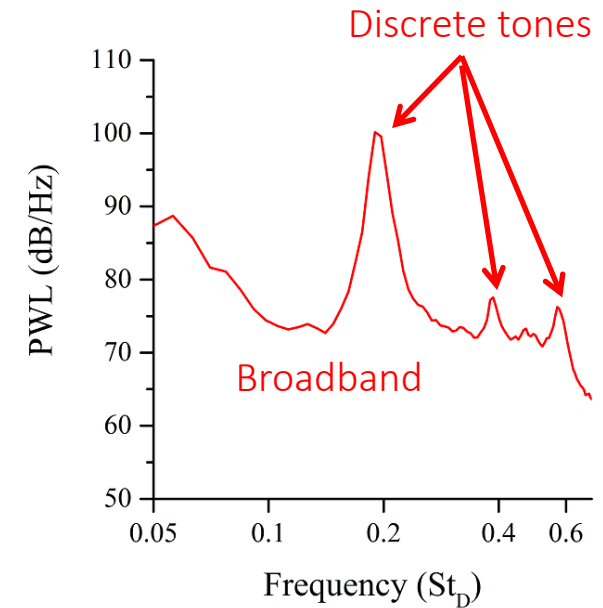
KLM Embraer 190 , powered by GE CF34-10E5



Rod-airfoil configuration



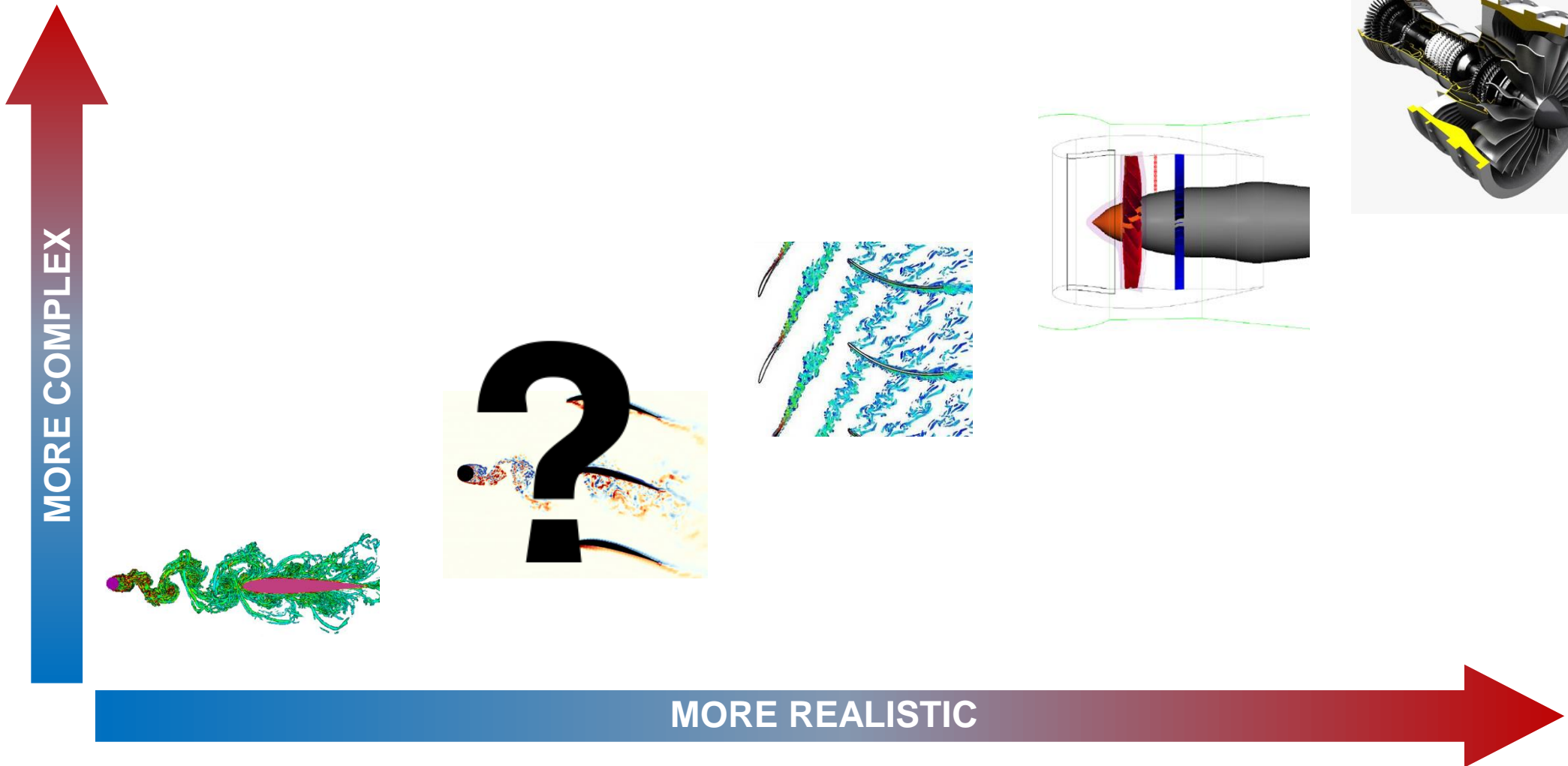
Typical turbofan noise power spectra [1]



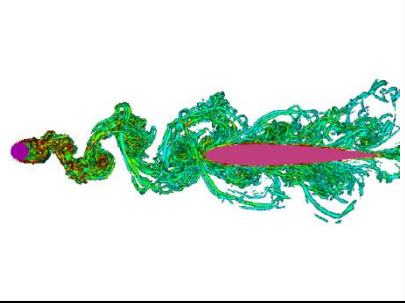
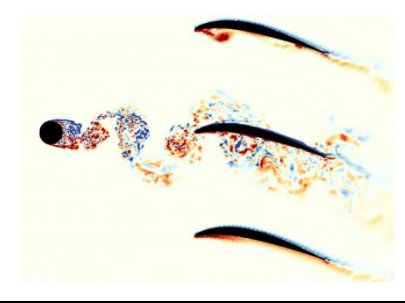
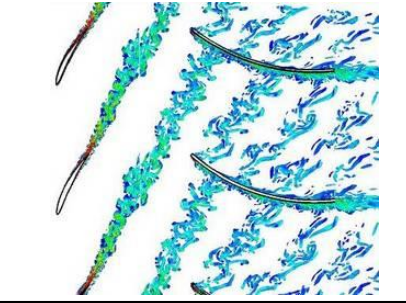
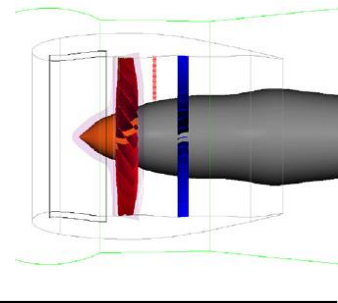
















Typical rod-airfoil configuration noise power spectra

[1] Hubbard, H. H.. *Aeroacoustics Of Flight Vehicles: Theory And Practice. Volume 1. Noise Sources* (No. NASA-L-16926-VOL-1). NASA Langley Research Center Hampton, VA. 1991.

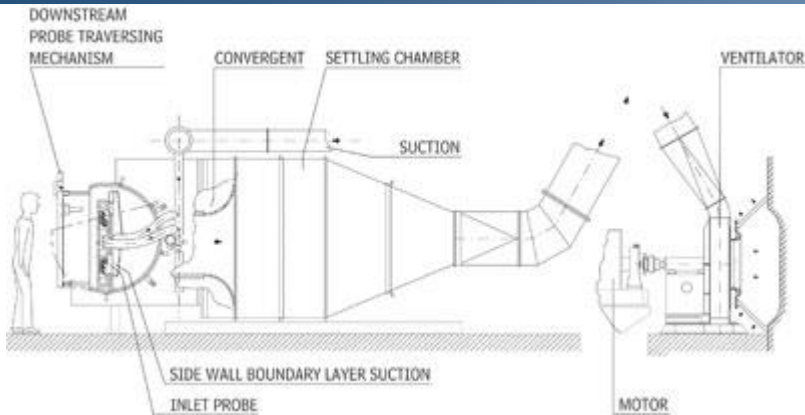
THE BRIDGE TOWARDS REALISM



A CONFIGURATION TO FILL THE GAP

				
Tonal and broadband excitation as source				
Flow deflection (cascade flow field) and acoustic-blade interaction				
Multiple blade excitation and source phase interference				
Rotor swirl and duct mode propagation				

CASCADE / HIGH-DEFLECTION WIND TUNNEL



C-1 Wind Tunnel, VKI, Belgium [1]



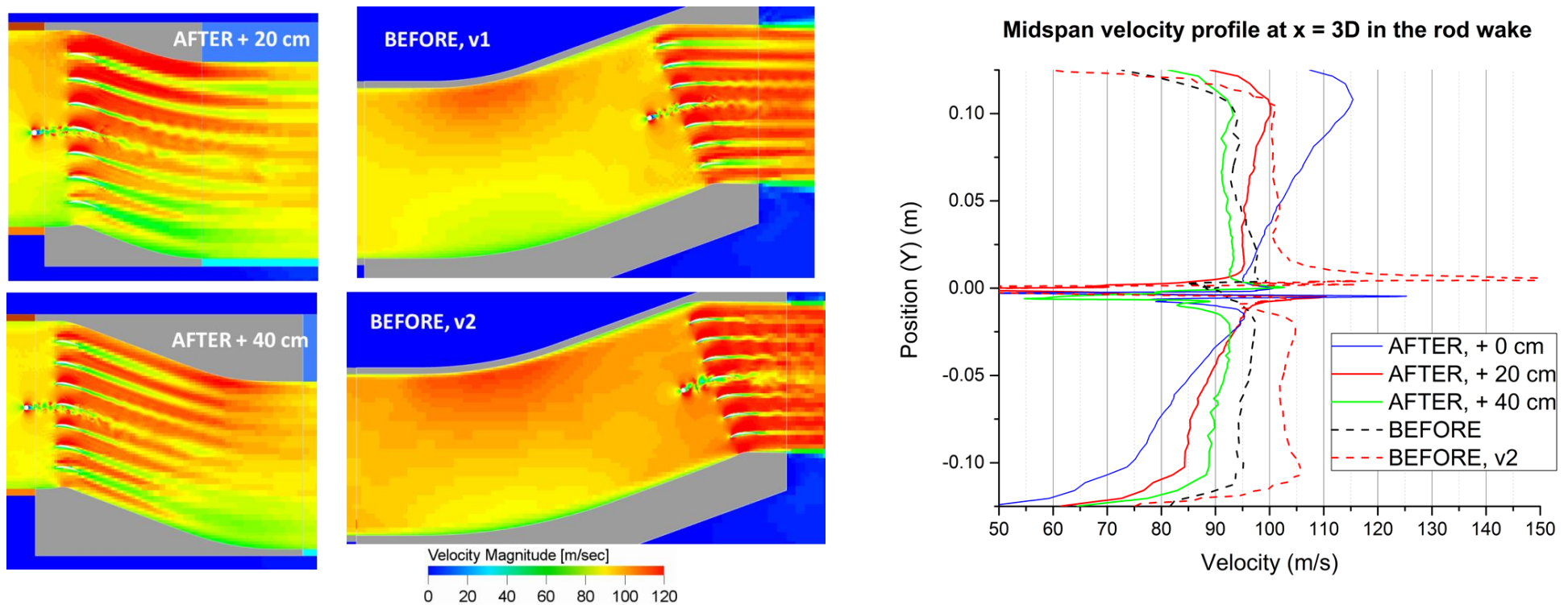
NGG Tunnel, DLR, Germany [2]

[1] <https://www.vki.ac.be/index.php/research-consulting-mainmenu-107/facilities-other-menu-148/turbomachinery-other-menu-174/86-low-speed-cascade-wind-tunnel-c-1>

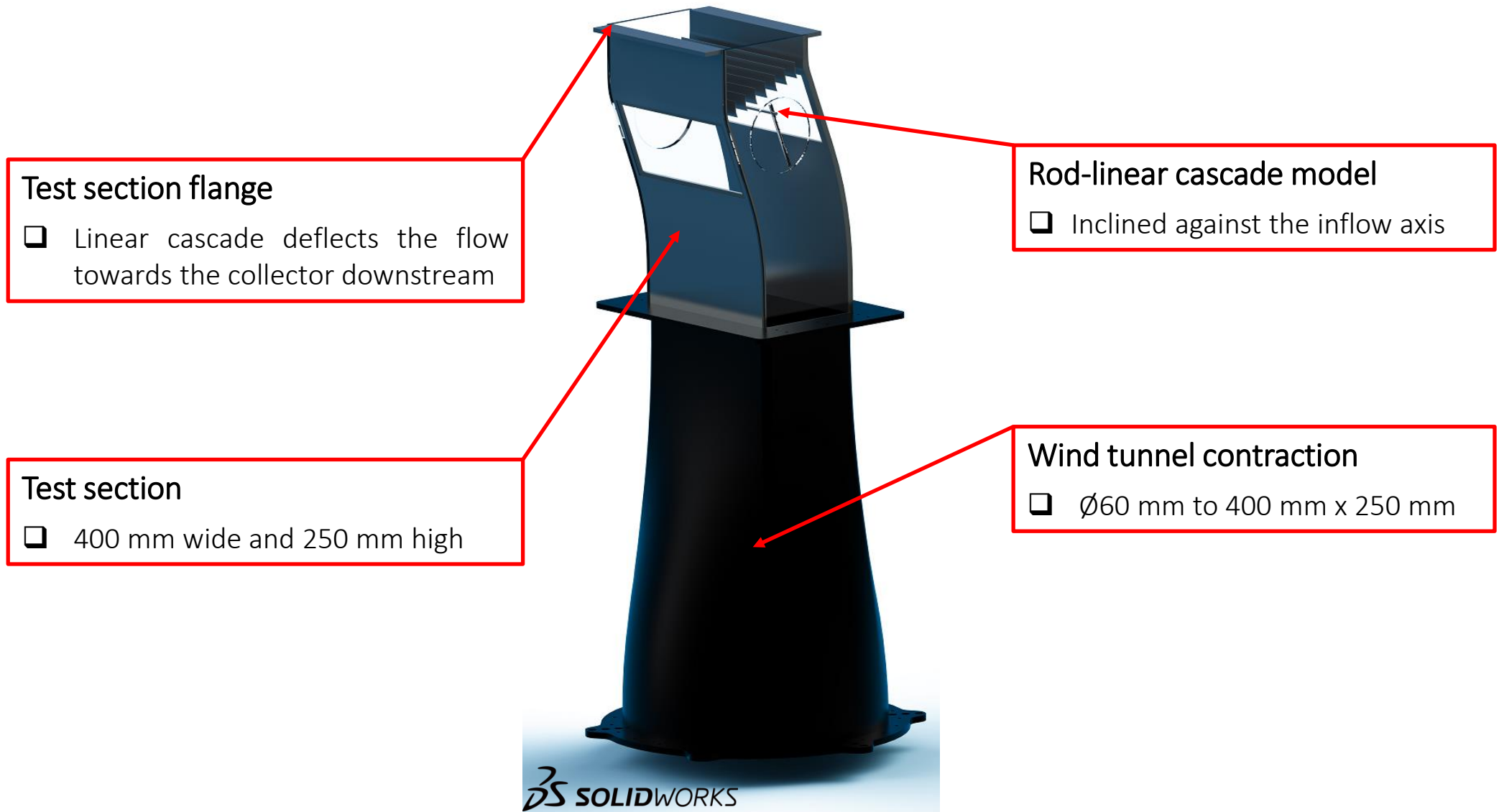
[2] https://www.dlr.de/at/en/desktopdefault.aspx/tabid-1562/2429_read-3782/.

DEFLECT THE FLOW BEFORE OR AFTER THE CASCADE?

- Flow exiting the test section must be aligned with the collector downstream.

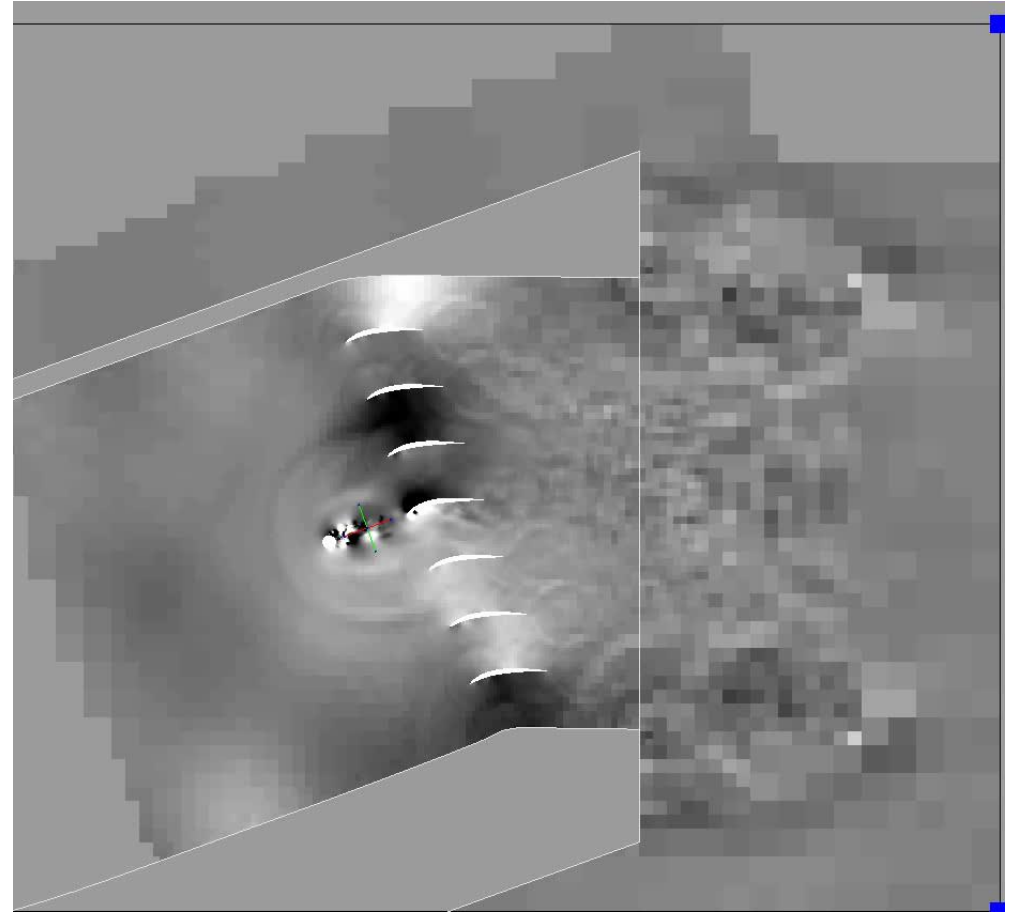
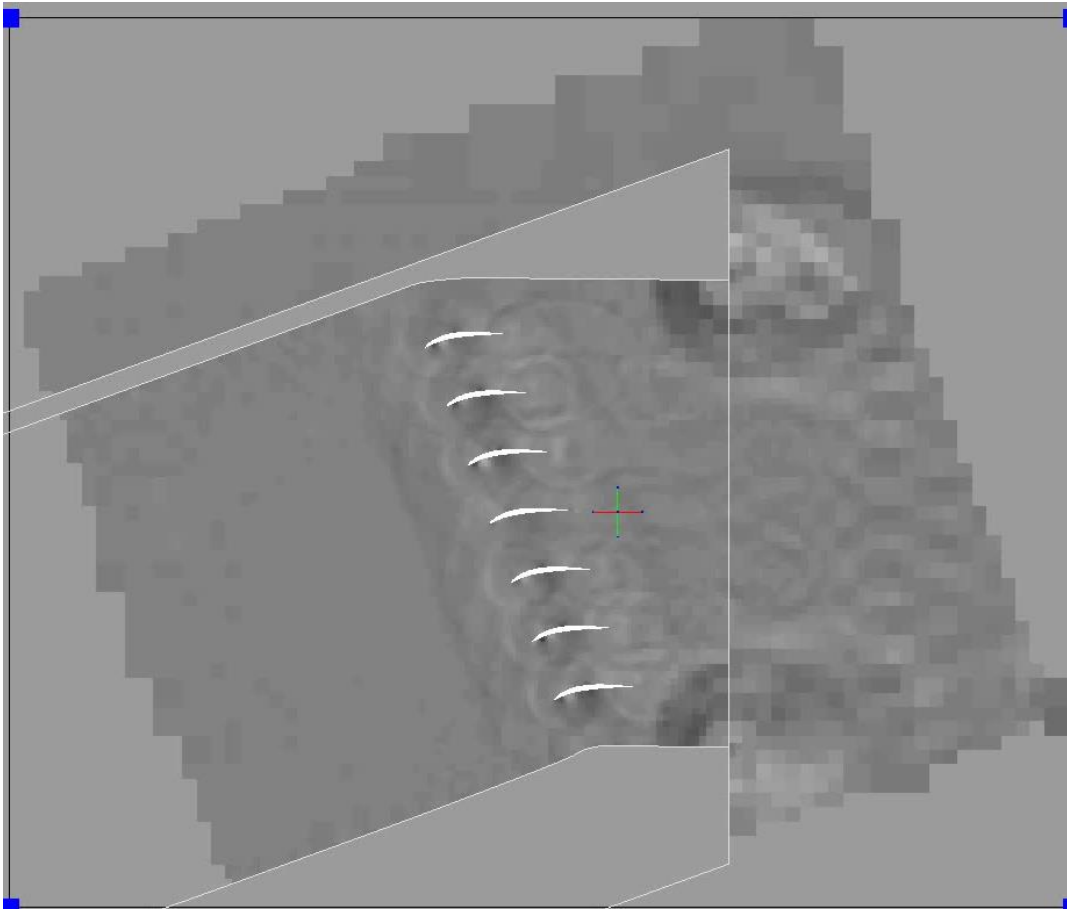


Parametric simulations to achieve acceptable flow uniformity within the test section



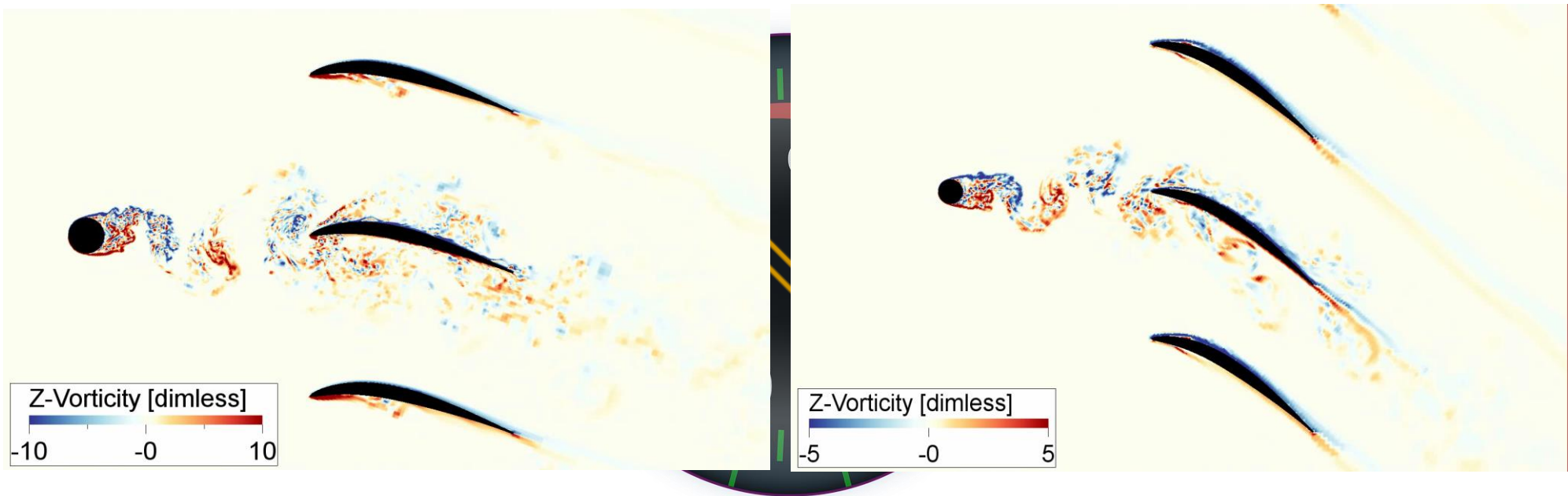
Rod-linear cascade experimental rig

ONE ROD TO MAKE THE DIFFERENCE

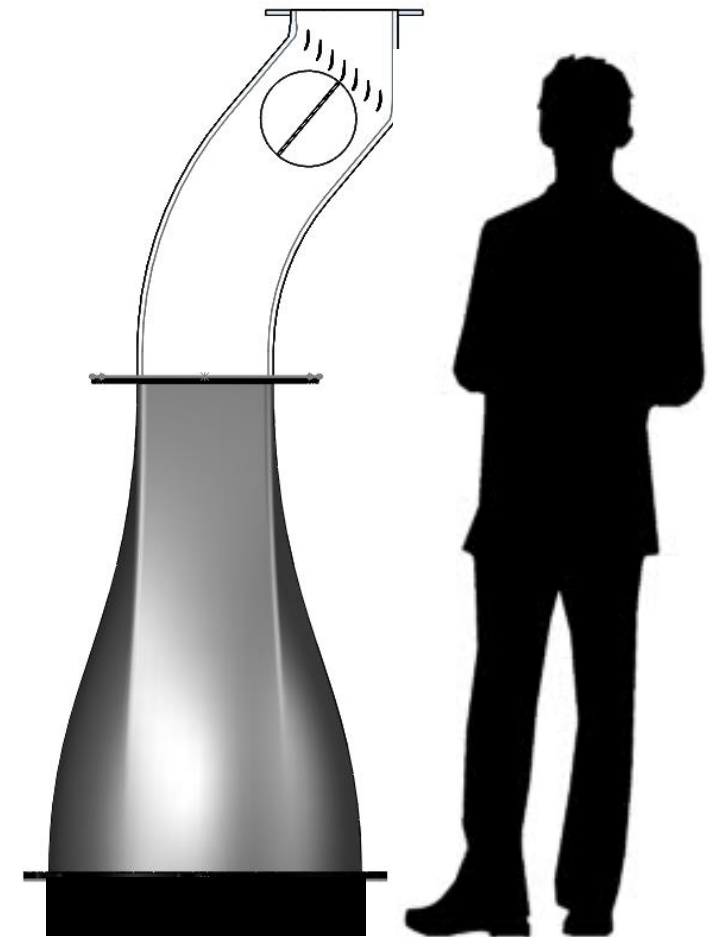


Comparison of linear cascade acoustics response with and without rod-wake excitation

- Overestimated wind tunnel capability
 - Freestream velocity is readjusted from 100 m/s to 75 m/s
- Unwanted separation on the cascade blade
 - Cascade incidence is increased from 10.5° to 30° (operational condition)

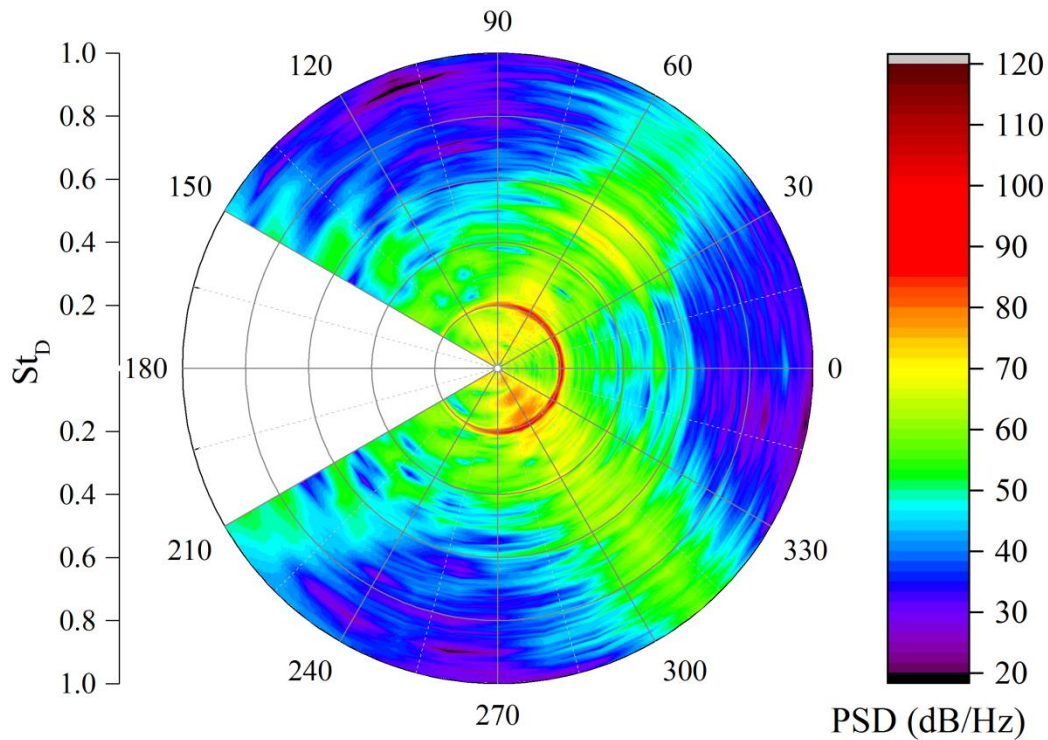


FULLY-MODULAR TEST RIG

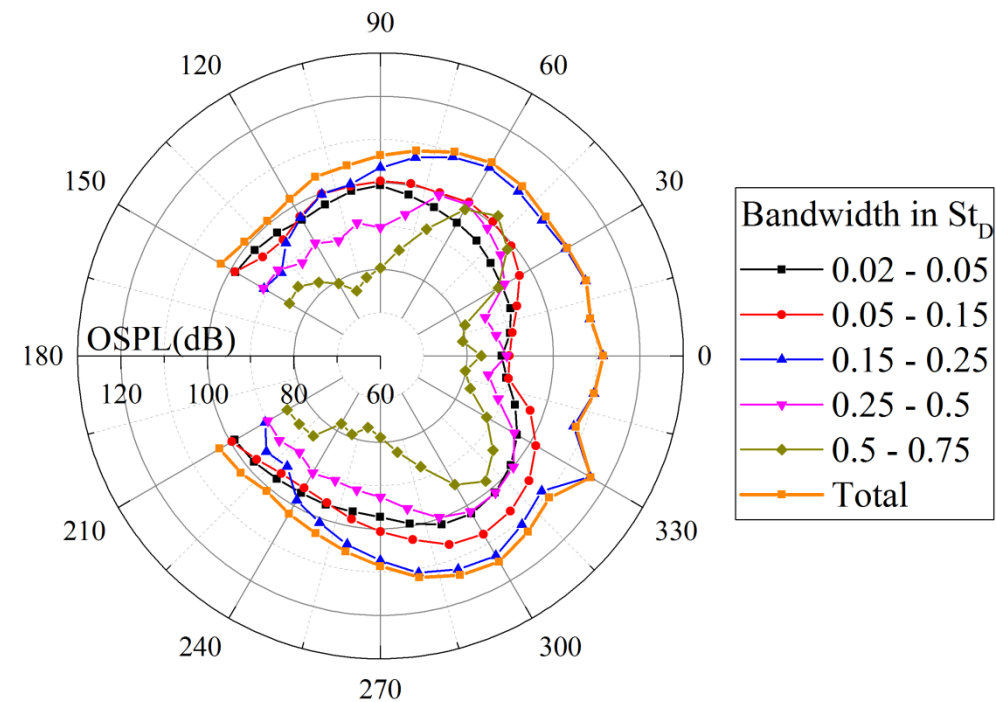


The test rig to human scale comparison

II. PRELIMINARY RESULTS

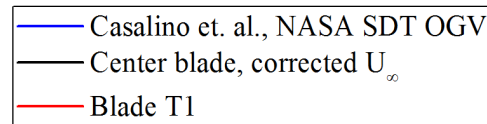
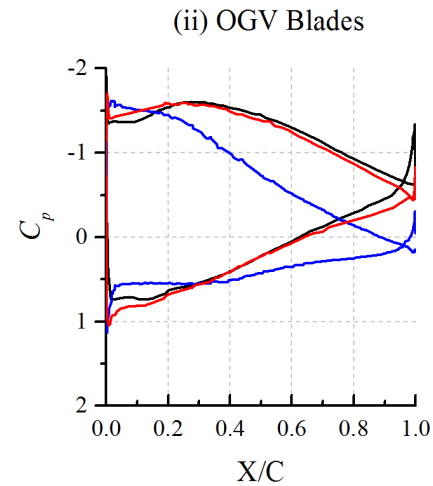
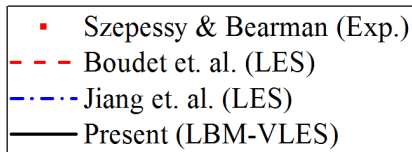
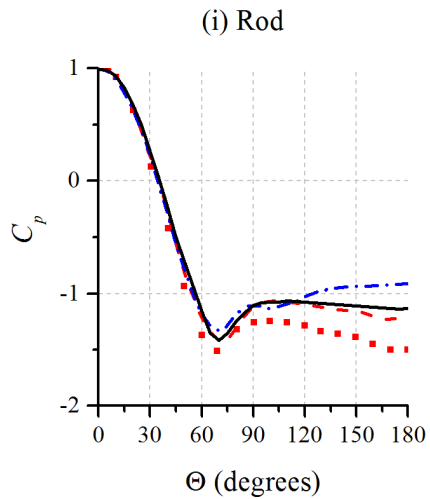


Power Spectral Density Directivity

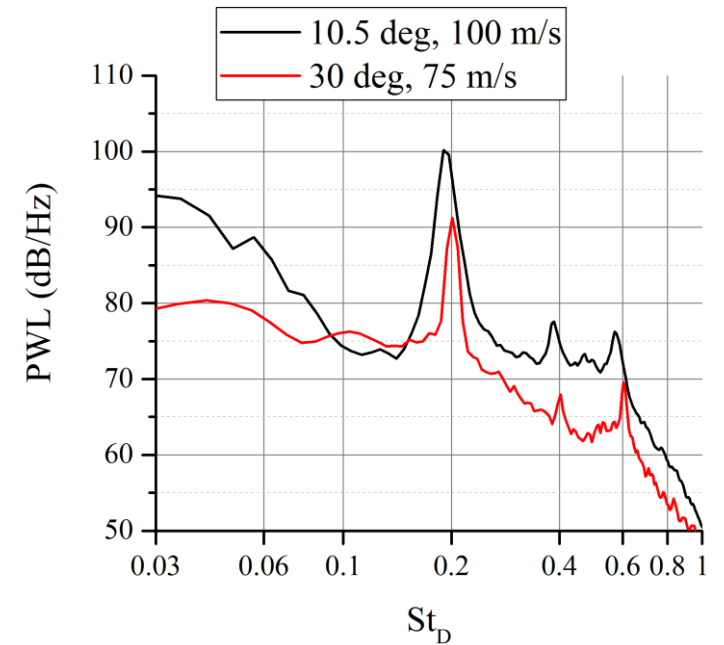


Narrowband OSPL Directivity

- The narrowband at the BPF dominates the OSPL in most direction.
- **Very narrow directivity** for the broadband components at **higher frequency ranges**, which may corresponds to the **diffraction of turbulent eddies** by the blade edges.

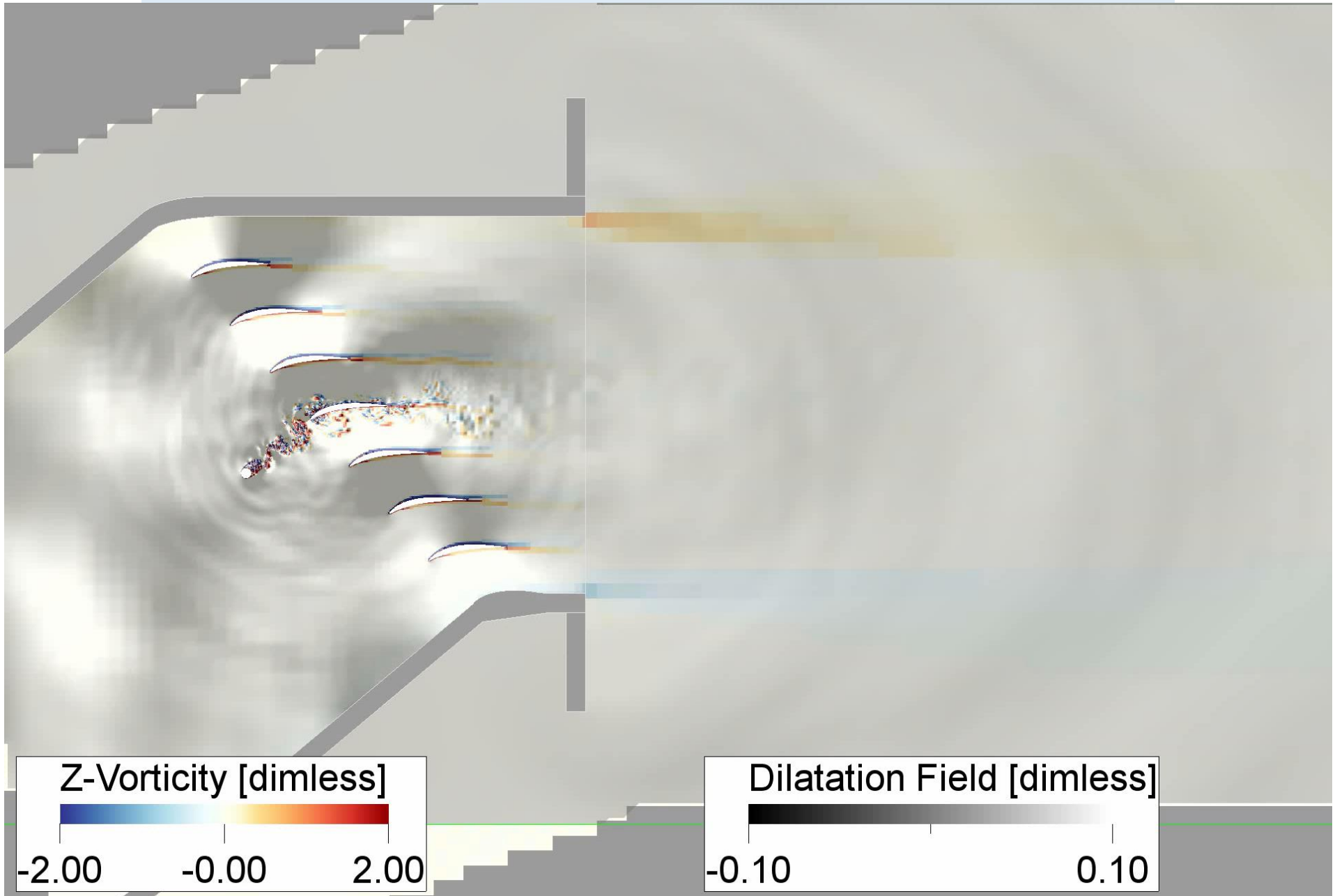


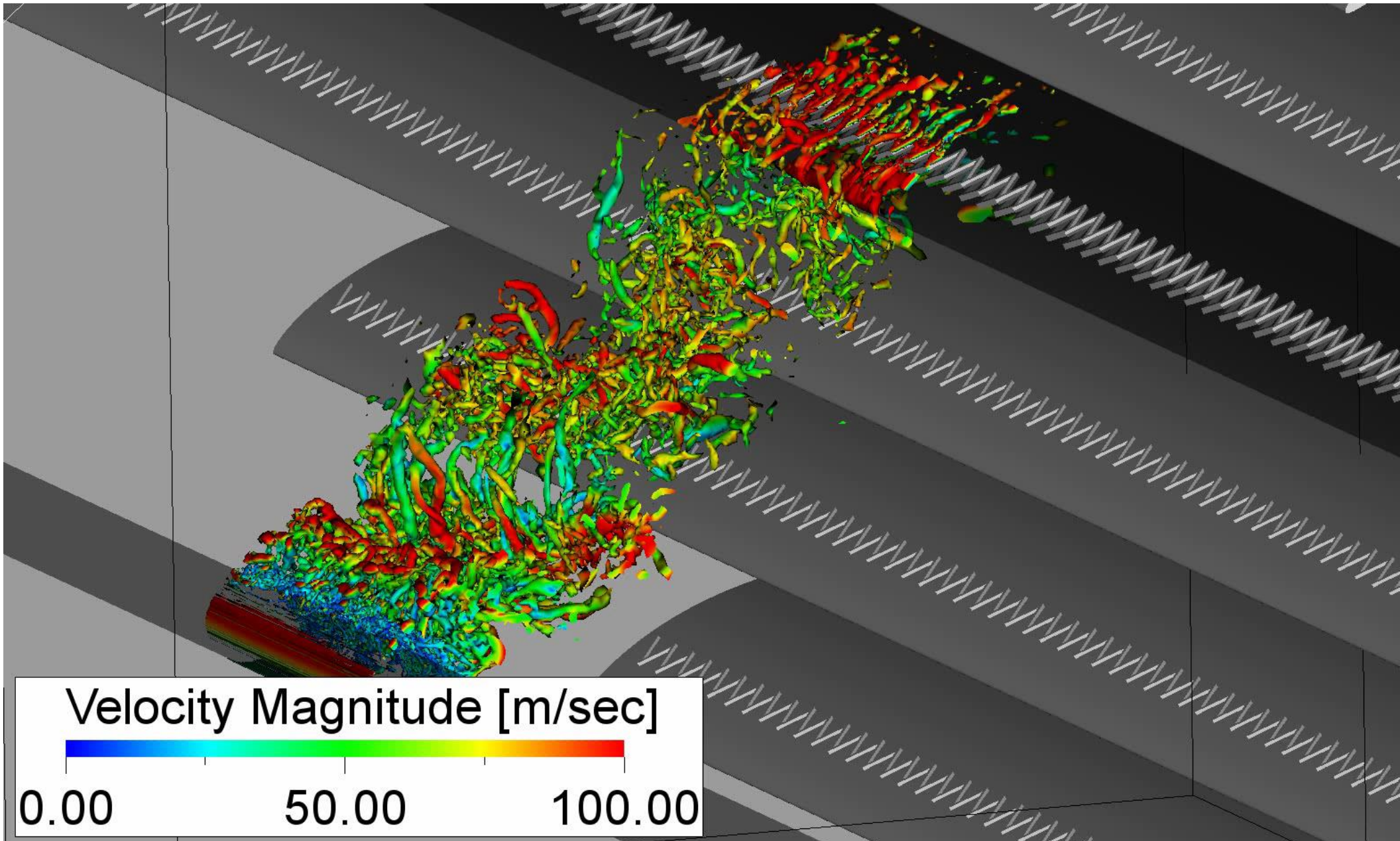
Pressure distribution on rod and OGV surface



Source power level comparison

- Source PWL is reduced due to lower freestream velocity. Better SNR at the BPF due to weaker low-frequency contents.
- Discrepancy in the blade pressure distribution is very likely due to stagger angle difference.

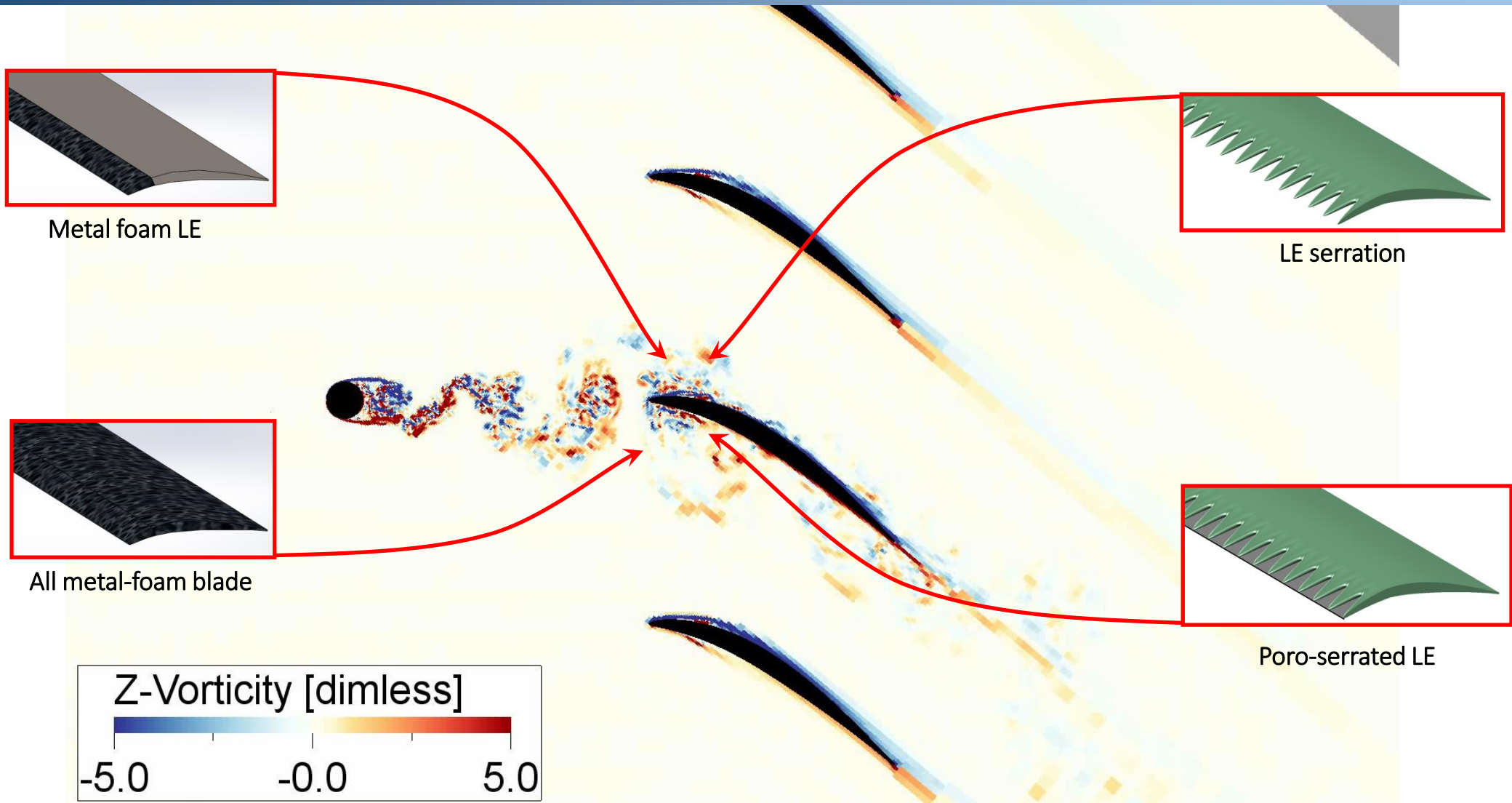






V. OUTLOOK

A FLEXIBLE PLATFORM FOR *TIN* MITIGATION STUDIES



- Experimental campaign to verify the simulations.
- The inclusion of leading edge serration to the OGV as baseline noise mitigation strategy and to investigate its impacts on performance.
- Characterization of metal-foam sample with PowerFLOW porous media models.





Thank you for your attention !

