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#### Context and motivations

- ORC industry looks toward more CFD based designs
- Turbulence is known to be at the origin of a significant amount of the turbine losses (see Wheeler's team work)
- No dedicated turbulence model exists for dense gas flows.



French Research Agency (ANR)
Young Researcher project
EDGES



### EDGES Program (2018-2022)

- Context: A few words on EDGES Program (2018-2022)
  - A DNS database for the analysis of turbulence in DG flows
- A bit of theory: Turbulence subgrid-scale (sgs) terms in DG flows and the issue of total energy
- Analysis of sgs terms in HIT and mixing layer
  - The example of sgs pressure
- Towards modeling of sgs pressure
  - Correlation based model
  - Neural network model

Conclusion

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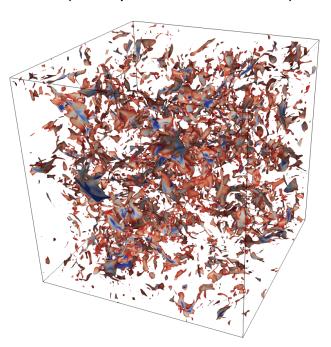
#### Context and motivations

- The ANR Young Researcher EDGES project (2018-2022):
  - 4 researchers over 4 years
- WP1 : Production of a DNS database of turbulent dense gas flows
- WP2: A-priori analysis of LES and RANS turbulence closure models
- WP3 : Development of new models for RANS and LES methods
- WP4: LES and RANS simulation of a realistic ORC turbine (a-posteriori validation)



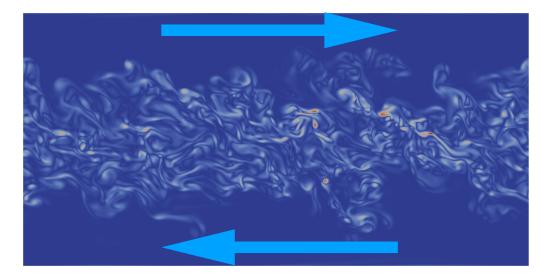
### A DNS database for the analysis of turbulence in DG flows

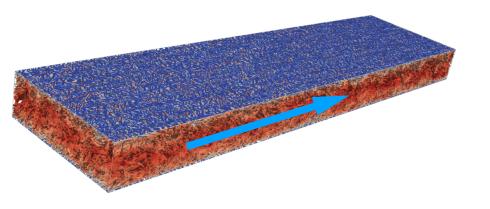
 Forced and free HIT (Giauque et al., JoT 2020)



Channel flows
 Grand challenge TGCC
 (P Errante)

 Mixing Layers (Vadrot et al., JFM 2020) (Vadrot et al., 2021 submitted to JFM)







#### **Outline**

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# The issue of total energy in LES (a debate from the 90's)

When filtered, total energy in a perfect gas (PG) writes as

$$\bar{\rho}\tilde{E} = \frac{\bar{p}}{\gamma - 1} + \frac{1}{2}\bar{\rho}\tilde{u}_i\tilde{u}_i + \frac{\tau_{ii}}{2}$$

 Which shows that even in PG, when Vreman (1995) writes a transport equation for

$$\bar{\rho}\hat{E} = \frac{\bar{p}}{\gamma - 1} + \frac{1}{2}\bar{\rho}\tilde{u}_i\tilde{u}_i$$

it is not a conservation equation because some energy lies at the subgrid-scale

$$ar{f}$$
 Reynolds average  $\label{eq:f_f} ilde{f} = rac{\overline{
ho f}}{ar{
ho}}$  Favre average

$$\hat{f} = f(\bar{\rho}, \tilde{u}_i, \tilde{E})$$
 Quantity computed using only filtered fields



### The issue of total energy in LES (a debate from the 90's)

 The fact is, not many people care and most often one assumes that since

$$\frac{1}{2}(\widetilde{u_iu_i} - \widetilde{u_i}\widetilde{u_i}) \ll \widetilde{E_{int}} \implies \widetilde{E} \approx \widehat{E}$$

 The main reason is that given the simplicity of the EoS equation, the following equalities stand

$$\bar{\rho}\tilde{E}_{int} = \frac{\bar{p}}{\gamma - 1} = C_{\nu}\bar{\rho}\tilde{T}$$

In PG, thermodynamics does not care about filtering and the difference for total energy only lies in sgs velocity correlations  $\frac{1}{2}(\widetilde{u_iu_i} - \widetilde{u_i}\widetilde{u_i})$ 

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# The issue of total energy in LES in dense gas

In dense gas, internal energy is influenced by the filtering

$$\tilde{E} \neq E(\bar{\rho}, \bar{P})$$

or equivalently

$$\bar{P} \neq P(\bar{\rho}, \tilde{E})$$

In DG, thermodynamics is influenced by the filtering



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- A-priori analysis of sgs terms in HIT and mixing layer
  - The example of the momentum equation and sgs pressure
- Towards modeling of sgs pressure
  - Regression models
  - Neural network model

Conclusion



To illustrate our results will now concentrate on the momentum equation

$$\frac{\partial \bar{\rho}\tilde{u}_{i}}{\partial t} = \underbrace{\left(\frac{\partial \hat{p}}{\partial x_{i}}\right)} - \frac{\partial (\bar{p} - \hat{p})}{\partial x_{i}} + \frac{\partial \hat{\tau}_{ij}}{\partial x_{j}} + \frac{\partial (\bar{\tau}_{ij} - \hat{\tau}_{ij})}{\partial x_{j}} - \frac{\partial \bar{\rho}\tilde{u}_{i}\tilde{u}_{j}}{\partial x_{j}} - \frac{\partial \bar{\rho}(\tilde{u}_{i}u_{j} - \tilde{u}_{i}\tilde{u}_{j})}{\partial x_{j}}$$

**Pressure: Main** 



To illustrate our results will now concentrate on the momentum equation

$$\frac{\partial \bar{\rho}\tilde{u}_{i}}{\partial t} = -\frac{\partial \hat{p}}{\partial x_{i}} - \frac{\partial (\bar{p} - \hat{p})}{\partial x_{i}} + \underbrace{\begin{pmatrix} \partial \hat{\tau}_{ij} \\ \partial x_{j} \end{pmatrix}}_{\partial x_{j}} + \underbrace{\frac{\partial (\bar{\tau}_{ij} - \hat{\tau}_{ij})}{\partial x_{j}}}_{\partial x_{j}} - \underbrace{\frac{\partial \bar{\rho}\tilde{u}_{i}\tilde{u}_{j}}{\partial x_{j}}}_{\partial x_{j}} - \underbrace{\frac{\partial \bar{\rho}\tilde{u}_{i}\tilde{u}_{j}}{\partial x_{j}}}_{\partial x_{j}} - \underbrace{\frac{\partial \bar{\rho}\tilde{u}_{i}\tilde{u}_{j}}{\partial x_{j}}}_{\partial x_{j}}$$

Tau: Main



To illustrate our results will now concentrate on the momentum equation

$$\frac{\partial \bar{\rho}\tilde{u}_{i}}{\partial t} = -\frac{\partial \hat{p}}{\partial x_{i}} - \frac{\partial (\bar{p} - \hat{p})}{\partial x_{i}} + \frac{\partial \hat{\tau}_{ij}}{\partial x_{j}} + \frac{\partial (\bar{\tau}_{ij} - \hat{\tau}_{ij})}{\partial x_{j}} \underbrace{\left(\frac{\partial \bar{\rho}\tilde{u}_{i}\tilde{u}_{j}}{\partial x_{i}}\right)}_{\partial x_{i}} \frac{\partial \bar{\rho}(\tilde{u}_{i}u_{j} - \tilde{u}_{i}\tilde{u}_{j})}{\partial x_{i}}$$

**Convective: Main** 



To illustrate our results will now concentrate on the momentum equation

$$\frac{\partial \bar{\rho}\tilde{u}_{i}}{\partial t} = -\frac{\partial \hat{p}}{\partial x_{i}} \left( \frac{\partial (\bar{p} - \hat{p})}{\partial x_{i}} \right) + \frac{\partial \hat{\tau}_{ij}}{\partial x_{j}} + \frac{\partial (\bar{\tau}_{ij} - \hat{\tau}_{ij})}{\partial x_{j}} - \frac{\partial \bar{\rho}\tilde{u}_{i}\tilde{u}_{j}}{\partial x_{j}} - \frac{\partial \bar{\rho}(\tilde{u}_{i}u_{j} - \tilde{u}_{i}\tilde{u}_{j})}{\partial x_{i}} \right)$$

**Pressure: sgs** 

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To illustrate our results will now concentrate on the momentum equation

$$\frac{\partial \bar{\rho}\tilde{u}_{i}}{\partial t} = -\frac{\partial \hat{p}}{\partial x_{i}} - \frac{\partial (\bar{p} - \hat{p})}{\partial x_{i}} + \frac{\partial \hat{\tau}_{ij}}{\partial x_{j}} + \frac{\partial (\bar{\tau}_{ij} - \hat{\tau}_{ij})}{\partial x_{j}} - \frac{\partial \bar{\rho}\tilde{u}_{i}\tilde{u}_{j}}{\partial x_{j}} - \frac{\partial \bar{\rho}(\tilde{u}_{i}u_{j} - \tilde{u}_{i}\tilde{u}_{j})}{\partial x_{i}}$$

Tau: sgs



To illustrate our results will now concentrate on the momentum equation

$$\frac{\partial \bar{\rho}\tilde{u}_{i}}{\partial t} = -\frac{\partial \hat{p}}{\partial x_{i}} - \frac{\partial (\bar{p} - \hat{p})}{\partial x_{i}} + \frac{\partial \hat{\tau}_{ij}}{\partial x_{j}} + \frac{\partial (\bar{\tau}_{ij} - \hat{\tau}_{ij})}{\partial x_{j}} - \frac{\partial \bar{\rho}\tilde{u}_{i}\tilde{u}_{j}}{\partial x_{j}} \underbrace{\begin{pmatrix} \partial \bar{\rho}(\tilde{u}_{i}u_{j} - \tilde{u}_{i}\tilde{u}_{j}) \\ \partial x_{j} \end{pmatrix}}_{\partial x_{j}}$$

**Convective: sgs** 



- To determine the importance of the different terms in the momentum equation, we filter the DNS fields between:
  - $k = k_{min}$  which corresponds to a very large scale filter of size L
  - $k = k_{max}$  which corresponds to no filtering (scale is equal to  $2\Delta x$ )
- Note that in this case  $\bar{f}, \tilde{f}, \hat{f}$  should be denoted  $\bar{f}^k, \tilde{f}^k, \hat{f}^k$

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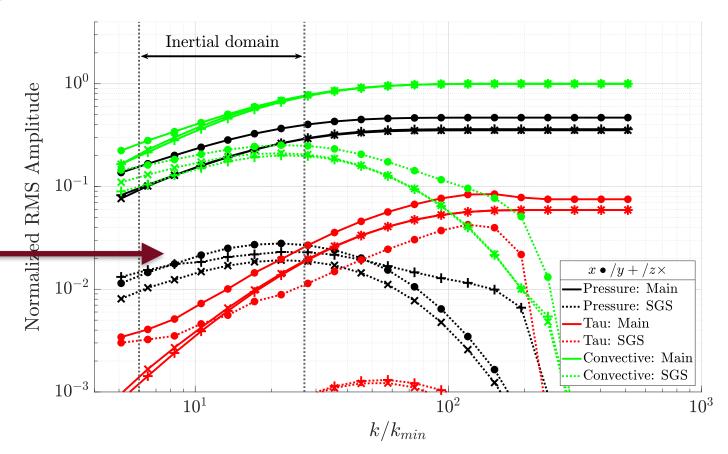


 We finally compute the rms amplitude of each term in the volume for each filtering wavenumber.

Pressure main term = 
$$\left( \left\langle \left[ \frac{\partial \hat{p}}{\partial x_i} \right]^2 \right\rangle_V - \left\langle \frac{\partial \hat{p}}{\partial x_i} \right\rangle_V^2 \right)^{1/2}$$



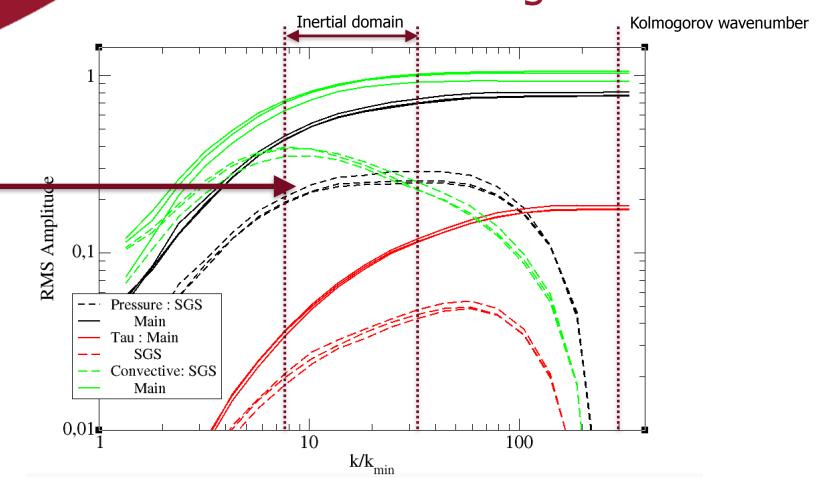
#### DG sgs terms- Mixing layer



 The pressure sgs term is larger than the main resolved viscous term



### DG sgs terms- HIT



 The pressure sgs term is of the order of the usual convective sgs term!



### The example of sgs pressure

We now concentrate on the subgrid-scale pressure in HIT.

$$p_{sgs} = \bar{p} - \hat{p} \left( \bar{\rho}, \overline{\rho E} \right)$$

•  $p_{sgs}$  changes with the filter size. We choose

$$l = L/15 \equiv k/k_{min} = 15$$

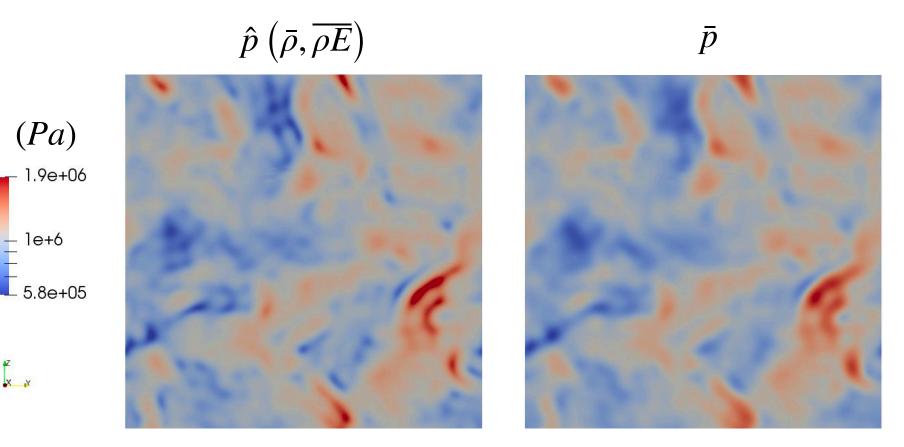
as it lies in the inertial range of turbulence where stronger correlations between filtered fields and sgs fields are expected

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### The example of sgs pressure in HIT

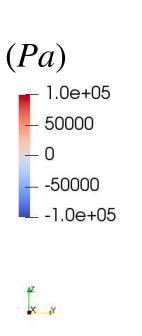
•  $\hat{p}$   $(\bar{\rho}, \bar{\rho}E)$  shows differences with  $\bar{P}$  especially in regions of strong gradients which are more sensitive to the filtering

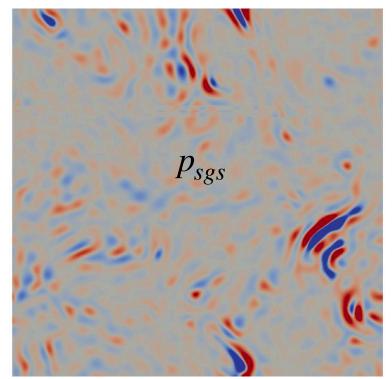




### The example of sgs pressure in HIT

• As expected  $P_{sgs}$  character length lies below the filtering size. Yet structures of larger sizes also appear related to region of strong gradients.





$$(l = L) \equiv (k/k_{min} = 1)$$
675 grid cells

$$(l = L/15) \equiv (k/k_{min} = 15)$$

$$45 \text{ grid cells}$$



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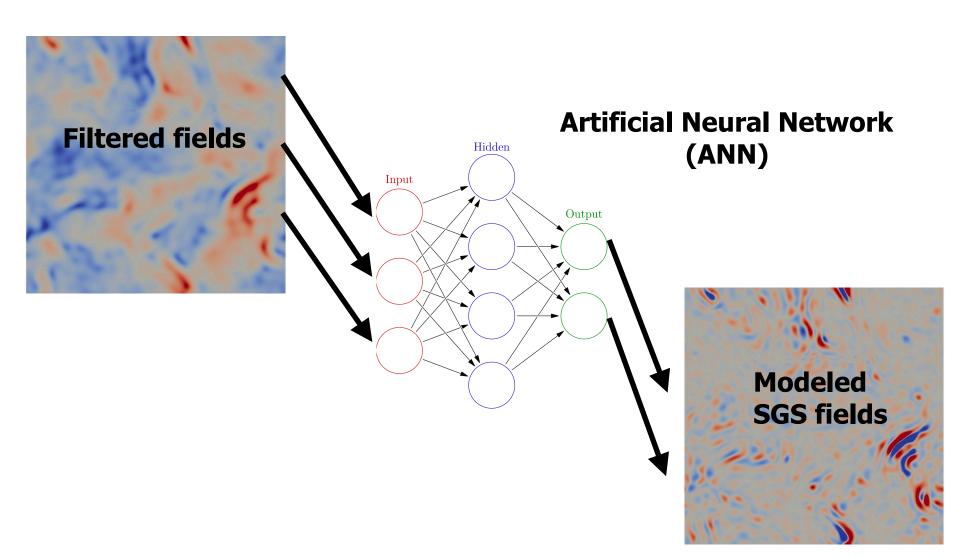


# Towards modeling of sgs pressure — Constraints

- Constraints are imposed to the modeling strategy:
  - Only quantities accessible to the future LES are used as inputs.
    - Only filtered fields are used as inputs
  - The model should be invariant by translation and rotation
    - Only variables independent of the coordinate system are used
  - To be efficient, the model should be local in space and time
    - No history is taken into account
    - The model at location x is obtained from fields at the same location x (no space convolution)
  - The model should be as independent as possible from the types of flows present in the DNS database.
    - All datasets (HIT, Mixing layer, Channel) will be used during training



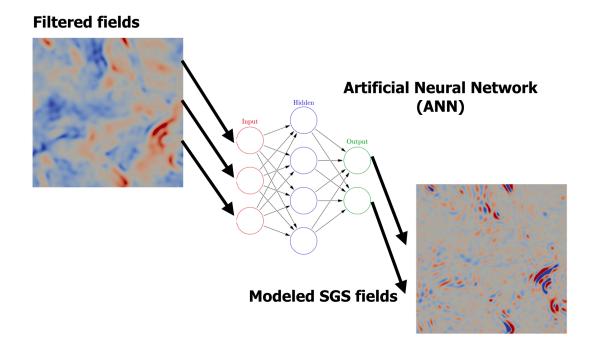
# Towards modeling of sgs pressure — Machine Learning





# Towards modeling of sgs pressure — ANN example

- Let's switch to Jupyter and see how ANN regression for sgs fields prediction can be easily implemented using tensorflow?
  - For those interested in the notebook, feel free to contact me!





### Towards modeling of sgs pressure — ANN example

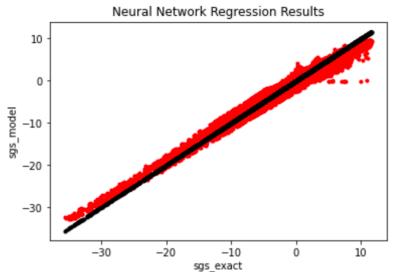
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- Using Parallel libraries, larger networks and large database (300M points), the correlation improves to 0.95 and R2 to 0.9.
- R2 of 0.9 means that 90% of the variance of the sgs term can be explained by the filtered fields.

Model Performance:

Correlation: 0.9569431616360217

0.9066780541374565





### Towards modeling of sgs pressure — Incoming challenges

- (WIP) further HPC implementation of the ANN training and optimize the architecture
- (TBD) Cross case (HIT, Mixing Layer, Channel) training and validation
- (TBD) Feature simplification using only the most influential parameters (network pruning using output of random forest)

a-posteriori validation thanks to available experimental results!



### Towards subgrid-scales turbulence modeling in dense gas flows

Thank you for your attention Questions?